

PART - A:

A1: Point form: $(\nabla \cdot \vec{J}) = -\frac{\partial \rho_v}{\partial t}$ (1)

Integral form: $\oint_s \vec{J} \cdot d\vec{s} = -\frac{dQ_i}{dt}$ (1)

A2: Point form of ohms law:

The relationship between \vec{J} and \vec{E} can also be expressed in terms of conductivity of the material

$$\vec{J} = \sigma \vec{E}$$

A3: Properties of dielectric material: (Any two)

1. The dielectric do not contain any free charges but contain bound charges.
2. Bound charges are under the internal molecular and atomic forces and cannot contribute to the conduction.
3. Due to the polarization, the dielectrics can store the energy.
4. Due to the polarization, the flux density of the dielectric increases by amount equal to the polarization.
5. The induced dipoles produce their own electric field and align in the direction of the applied electric field.
6. The electric field outside and inside the dielectric gets modified due to the induced electric dipoles.
7. Due to electric field \vec{E} , small electric dipoles gets induced inside the dielectric. This is called polarization.

A4:

$$E_{tan} = D_{tan} = 0$$

$$D_N = \rho_s$$

$$E_N = \frac{\rho_s}{\epsilon} = \frac{\rho_s}{\epsilon_0 \epsilon_r}$$

A5: Uniqueness Theorem:

If the solution of Laplace's equation satisfies the boundary condition then that solution is unique, by whatever method it is obtained.

A6: curl:

The curl of a vector in the direction of the unit vector is the ratio of the line integral of a vector around a closed contour, to the enclosed area bounded by the contour, as the enclosed area tends to zero. (1)

$$\lim_{\Delta S_N \rightarrow 0} \frac{\oint \vec{H} \cdot d\vec{l}}{\Delta S_N} = J_N$$

Properties of curl: (Any two) (1)

1. The curl of a vector is a vector quantity
2. $\nabla \times (\vec{A} + \vec{B}) = \nabla \times \vec{A} + \nabla \times \vec{B}$
3. $\nabla \times \nabla \times \vec{A} = \nabla(\nabla \cdot \vec{A}) - \nabla^2 \vec{A}$
4. $\nabla \cdot (\nabla \times \vec{A}) = 0$
5. $\nabla \times \nabla \psi = 0$

A7: Amperes circuital law:

The line integral of magnetic field intensity \vec{H} around a closed path is exactly equal to the direct current enclosed by that path,

$$\oint \vec{H} \cdot d\vec{l} = I \quad (1)$$

Point form of Amp. circuital law:

$$\nabla \times \vec{H} = \vec{J} \quad (1)$$

A8: Self Inductance:

The ratio of total flux linkage to the current through the circuit is called inductance and it is given by (1)

$$L = \frac{N\Phi}{I}$$

The inductance is known as self inductance

The inductance is known as self inductance

Mutual Inductance:

(1)

(2)

The Mutual Inductance between the two circuit is defined as the flux linkage of one circuit to the current in the other circuit.

$$M = \frac{\text{Flux linkage of circuit 1}}{\text{current in circuit 2}}$$

A9:

Solution:

$$M = k \sqrt{L_1 L_2} = 0.05 \sqrt{800 \times 200} = 20 \mu H \quad (1)$$

$$L = L_1 + L_2 + 2M = 800 \times 10^{-6} + 200 \times 10^{-6} + 2 \times 20 \times 10^{-6}$$

$$L = 1040 \mu H$$

(1)

A10: Magnetic Torque:

(1)

The magnetic torque on the loop is defined as the vector product of the force (F) and the moment arm (r)

$$T = F \times r \quad N \cdot m$$

Magnetic Dipole:

(1)

The magnetic field which is having two poles and forms a closed loop is called magnetic dipole.

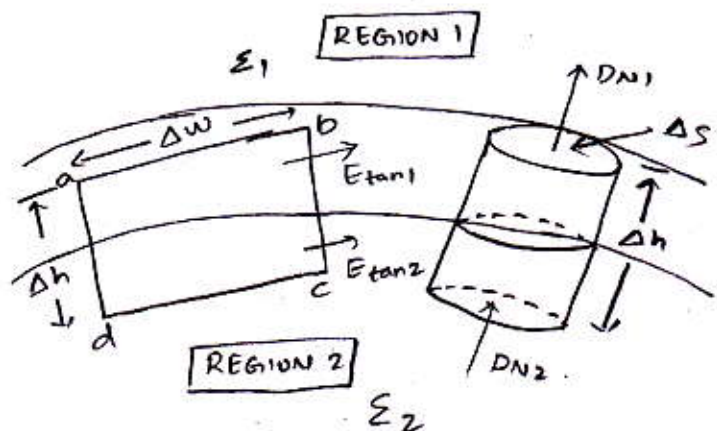
PART-B

B1) a) i) Boundary Conditions between Dielectric to Dielectric:

Tangential component:

$$\oint \vec{E} \cdot d\vec{l} = 0 \quad \text{--- (1)}$$

Evaluating the integral $\vec{E} \cdot d\vec{l}$ along the path a, b, c, d, a in clockwise direction.



$$\int_a^b \vec{E} \cdot d\vec{l} + \int_b^c \vec{E} \cdot d\vec{l} + \int_c^d \vec{E} \cdot d\vec{l} + \int_d^a \vec{E} \cdot d\vec{l} = 0 \quad \text{--- (2)}$$

Now, $\vec{E}_1 = \vec{E}_{1t} + \vec{E}_{1N}$

$$|\vec{E}_{1t}| = E_{1t}, \quad |\vec{E}_{1N}| = E_{1N}$$

$$\vec{E}_2 = \vec{E}_{2t} + \vec{E}_{2N}$$

$$|\vec{E}_{2t}| = E_{2t}, \quad |\vec{E}_{2N}| = E_{2N}$$

To analyse boundary condition, $\Delta h \rightarrow 0$

\therefore In eq (2) $\int_b^c \vec{E} \cdot d\vec{l} + \int_d^a \vec{E} \cdot d\vec{l} = 0$ as $\Delta h \rightarrow 0$

$\therefore \int_a^b \vec{E} \cdot d\vec{l} + \int_c^d \vec{E} \cdot d\vec{l} = 0 \quad \text{--- (3)}$

for a-b $\Rightarrow E = E_{1t} \quad dl = \Delta w$

for c-d $\Rightarrow E = E_{2t} \quad dl = \Delta w$

$$E_{1t}(\Delta w) - E_{2t} \Delta w = 0$$

(1)

$$\boxed{E_{1t} = E_{2t}}$$

w.k.t $\vec{D} = \epsilon \vec{E}$

$$D_{1t} = \epsilon_1 E_{1t}$$

$$D_{2t} = \epsilon_2 E_{2t}$$

$$\frac{D_{1t}}{\epsilon_1} = \frac{D_{2t}}{\epsilon_2}$$

$$\boxed{\frac{D_{1t}}{D_{2t}} = \frac{\epsilon_1}{\epsilon_2}}$$

(1)

Normal component: consider Gaussian Surface

$$\oint \vec{D} \cdot d\vec{s} = Q$$

$$\left[\int_{\text{top}} + \int_{\text{bottom}} + \int_{\text{lateral}} \right] \vec{D} \cdot d\vec{s} = Q$$

As $\Delta h \rightarrow 0$ $\int_{\text{lateral}} \vec{D} \cdot d\vec{s} = 0$

$$\left[\int_{\text{top}} + \int_{\text{bottom}} \right] \vec{D} \cdot d\vec{s} = Q$$

$$D_{N1} \Delta S - D_{N2} \Delta S = Q$$

But $Q = \rho_s \Delta S$

$$D_{N1} - D_{N2} = \rho_s$$

(1)

$\rho_s = 0$ for ideal dielectric, then

$$D_{N1} = D_{N2}$$

$$D_{N1} = \epsilon_1 E_{N1} \quad D_{N2} = \epsilon_2 E_{N2}$$

$$\frac{E_{N1}}{E_{N2}} = \frac{\epsilon_2}{\epsilon_1}$$

(1)

Conductor to Dielectric Medium

(2)

$$E_{tan} = D_{tan} = 0$$

$$D_N = \rho_s$$

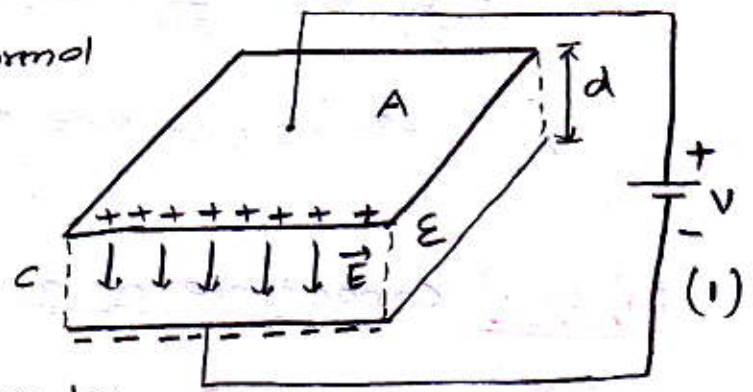
$$E_N = \frac{\rho_s}{\epsilon}$$

B1) a) ii)

Energy Stored in a Capacitor:

Let \vec{a}_N is the direction normal to the plates

$$\therefore \vec{E} = \frac{V}{d} \vec{a}_N$$



The energy stored is given by,

$$W_E = \frac{1}{2} \int_{Vol} \vec{D} \cdot \vec{E} \, dv$$

$$\vec{D} = \epsilon \vec{E} \quad (1)$$

$$= \frac{1}{2} \int_{Vol} \epsilon \vec{E} \cdot \vec{E} \, dv$$

$$\vec{E} \cdot \vec{E} = |\vec{E}|^2$$

$$= \frac{1}{2} \int_{Vol} \epsilon |\vec{E}|^2 \, dv$$

$$|\vec{E}| = \frac{V}{d} \quad (1)$$

$$= \frac{1}{2} \int_{Vol} \epsilon \left(\frac{V^2}{d^2} \right) \, dv$$

but $\int dV = \text{Volume} = A \times d$

$$W_E = \frac{1}{2} \epsilon \frac{V^2 A d}{d^2}$$

$$= \frac{1}{2} \frac{\epsilon A}{d} V^2 = \frac{1}{2} C V^2 \quad \left[\because C = \frac{\epsilon A}{d} \right]$$

$$\boxed{W_E = \frac{1}{2} C V^2}$$

(2)

B1) a) iii)

Given:

$$V = 2x^2 - 3y^2 + z^2$$

To find:

satisfies the Laplace equation or not

Solution:

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2} \quad (1)$$

$$= \frac{\partial^2}{\partial x^2} [2x^2 - 3y^2 + z^2] + \frac{\partial^2}{\partial y^2} [2x^2 - 3y^2 + z^2] + \frac{\partial^2}{\partial z^2} [2x^2 - 3y^2 + z^2] \quad (1)$$

$$= \frac{\partial}{\partial x} [4x] + \frac{\partial}{\partial y} [-6y] + \frac{\partial}{\partial z} [2z] = 4 - 6 + 2 = 0 \quad (2)$$

As, $\nabla^2 V = 0$, the field satisfies the Laplace equation.

B1) b) i) Capacitance of a parallel plate capacitor:

Let,

Q = charge on each plate

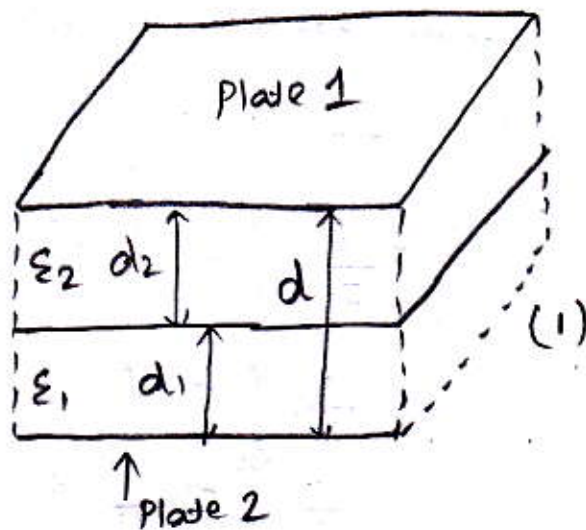
\vec{E}_1 = field intensity in region 1

\vec{E}_2 = field intensity in region 2

Both the intensities are uniform

$$V_1 = E_1 d_1$$

$$V_2 = E_2 d_2$$



$$V = V_1 + V_2 = E_1 d_1 + E_2 d_2 \quad \text{--- (1)}$$

(4)

At a dielectric - dielectric interface,

$$D_{N1} = D_{N2}$$

$$\text{Now } D_1 = \epsilon_1 E_1 \text{ \& } D_2 = \epsilon_2 E_2$$

$$E_1 = \frac{D_1}{\epsilon_1} \text{ \& } E_2 = \frac{D_2}{\epsilon_2} \quad \text{--- (2)}$$

Sub (2) in (1) we get

$$V = \frac{D_1}{\epsilon_1} d_1 + \frac{D_2}{\epsilon_2} d_2 \quad \text{--- (3)}$$

The magnitude of surface charge is same on each plate,

$$\therefore \rho_s = D_1 = D_2 \quad \text{--- (4)}$$

Sub eq (4) in eq (3)

$$V = \frac{\rho_s}{\epsilon_1} d_1 + \frac{\rho_s}{\epsilon_2} d_2 = \rho_s \left[\frac{d_1}{\epsilon_1} + \frac{d_2}{\epsilon_2} \right] \quad \text{--- (5) (2)}$$

$$\text{Now, } C = \frac{Q}{V} = \frac{Q}{\rho_s \left[\frac{d_1}{\epsilon_1} + \frac{d_2}{\epsilon_2} \right]} \quad (1)$$

$$\text{But } Q = \rho_s A$$

$$C = \frac{\rho_s A}{\rho_s \left[\frac{d_1}{\epsilon_1} + \frac{d_2}{\epsilon_2} \right]} = \frac{A}{\frac{d_1}{\epsilon_1} + \frac{d_2}{\epsilon_2}} = \frac{1}{\frac{d_1}{\epsilon_1 A} + \frac{d_2}{\epsilon_2 A}} \quad \boxed{\epsilon = \frac{1}{\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2}}} \quad (2)$$

$$\text{where, } C_1 = \frac{\epsilon_1 A}{d_1} \text{ \& } C_2 = \frac{\epsilon_2 A}{d_2}$$

B1) b) ii)

Given:

Diameter = 2 cm

a = radius of Sphere = $\frac{d}{2} = 1 \text{ cm} = 1 \times 10^{-2} \text{ m}$

$\epsilon_r = 2.26$

thickness = 3 cm

To Find:

capacitance

$$\text{Solution: } C = \frac{4\pi \epsilon_0 \epsilon_r a^2}{\frac{1}{\epsilon_1} \left(\frac{1}{a} - \frac{1}{r_1} \right) + \frac{1}{\epsilon_2}} \quad (2)$$

$$a = 1 \times 10^{-2} \text{ m}$$

$$r_1 = a + \text{thickness} = 1 + 3 = 4 \text{ cm} = 4 \times 10^{-2} \text{ m} \quad (1)$$

$$C = \frac{4\pi}{2.26 \left[\frac{1}{1 \times 10^{-2}} - \frac{1}{4 \times 10^{-2}} \right] + \frac{1}{8.854 \times 10^{-12} \times 4 \times 10^{-2}}} \quad (1)$$

$$C = 1.9121 \text{ PF} \quad (1)$$

B1) b) iii)

Poisson's and Laplace equation:

From the Gauss's law in the point form, Poisson's equation can be derived.

Consider the Gauss's law in the point form as

$$\nabla \cdot \vec{D} = \rho_v \quad \text{--- (1)}$$

$$\text{w.k.t } \vec{D} = \epsilon \vec{E} \quad \text{--- (2)}$$

$$\nabla \cdot \epsilon \vec{E} = \rho_v \quad \text{--- (3)}$$

$$\text{from gradient } \vec{E} = -\nabla V \quad \text{--- (4)}$$

Sub (4) in (3) we get

$$\nabla \cdot \epsilon (-\nabla V) = \rho_v$$

$$-\epsilon [\nabla \cdot \nabla V] = \rho_v$$

$$\nabla \cdot \nabla V = -\frac{\rho_v}{\epsilon} \quad \text{--- (5)}$$

$$\nabla^2 V = -\frac{\rho_v}{\epsilon} \quad \text{--- (6)} \quad (2)$$

Equation (6) is called Poisson's equation.

In certain region, $\rho_v = 0$

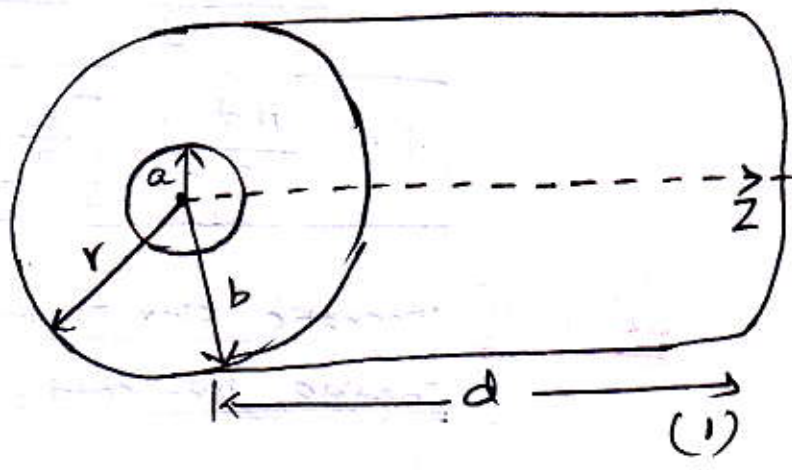
$$\nabla^2 V = 0 \quad (2)$$

This is a special case of Poisson's equation called as Laplace's equation.

B2) a) i) Inductance of a co-axial cable:

Magnetic field intensity at any point between inner and outer conductor is given by

$$\vec{H} = \frac{I}{2\pi r} \quad a < r < b$$



w.k.t $\vec{B} = \mu \vec{H}$

$$\vec{B} = \frac{\mu I}{2\pi r} \quad (1)$$

Axis of cable along z-axis $\therefore \vec{B}$ will be in radial plane extending from $r=a$ to $r=b$ and $z=0$ to $z=d$.

The total magnetic flux is given by

$$\phi = \int_S \vec{B} \cdot d\vec{s}$$

$$d\vec{s} = dr dz a\phi \quad (1)$$

$$\phi = \int_{z=0}^{z=d} \int_{r=a}^{r=b} \left(\frac{\mu I}{2\pi r} \right) a\phi (dr dz a\phi) \quad (1)$$

$$\phi = \int_{z=0}^d \int_{r=a}^b \frac{\mu I}{2\pi r} dr dz$$

$$\phi = \frac{\mu I}{2\pi} \int_{z=0}^d \int_{r=a}^b \frac{1}{r} dr dz$$

$$\phi = \frac{\mu I}{2\pi} [z]_0^d [\ln r]_a^b$$

$$\phi = \frac{\mu I d}{2\pi} \ln \left[\frac{b}{a} \right]$$

Inductance of a co-axial cable is given by

$$L = \frac{\text{Total Flux Linkage}}{\text{Total Current}} \quad (1)$$

$$L = \frac{\mu I d}{2\pi} \ln \left[\frac{b}{a} \right]$$

$$L = \frac{\mu d}{2\pi} \ln \left[\frac{b}{a} \right] \text{ Henry} \quad (1)$$

B2) a) ii) Magnetic Flux Intensity and density due to an
Infinite long conductor using Biot - Savart's Law:

Consider small differential element at Point 1, along the z-axis at a distance of z from origin,

$$\therefore \boxed{I d\vec{L} = I dz \vec{a}_z} \quad \text{--- (1)}$$

The distance vector joining Point 1 to point 2 is \vec{R}_{12}

$$\vec{R}_{12} = r\vec{a}_r + 0\vec{a}_\phi - z\vec{a}_z$$

$$\boxed{R_{12} = r\vec{a}_r - z\vec{a}_z} \quad \text{--- (2)}$$

$$\vec{a}_{R12} = \frac{\vec{R}_{12}}{|\vec{R}_{12}|} = \frac{-z\vec{a}_z + r\vec{a}_r}{\sqrt{r^2 + z^2}} = \frac{r\vec{a}_r - z\vec{a}_z}{\sqrt{r^2 + z^2}}$$

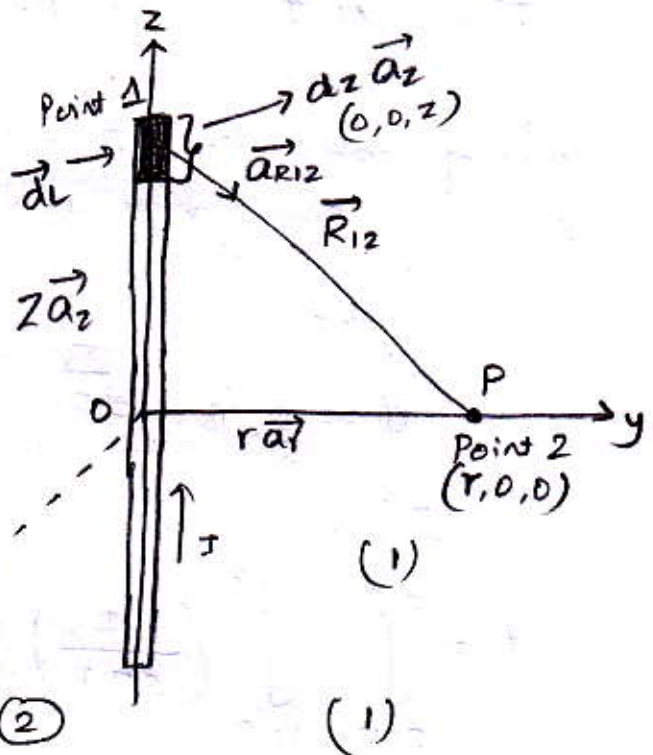
$$I d\vec{L} \times \vec{a}_{R12} = \frac{I r dz \vec{a}_\phi}{\sqrt{r^2 + z^2}}$$

According to Biot Savart's law, $d\vec{H}$ at point 2 is

$$d\vec{H} = \frac{I d\vec{L} \times \vec{a}_{R12}}{4\pi r^2} = \frac{I dz \times \vec{a}_z}{4\pi (r^2 + z^2)} \times \frac{r\vec{a}_r - z\vec{a}_z}{(\sqrt{r^2 + z^2})}$$

$$a_z \times a_r = a_\phi \quad a_z \times a_z = 0$$

$$\boxed{d\vec{H} = \frac{I r dz}{4\pi (r^2 + z^2)^{3/2}} a_\phi} \quad (1)$$



Thus total Flux intensity \vec{H} can be obtained by integrating $d\vec{H}$ over the entire length of the conductor

$$\vec{H} = \int_{z=-\infty}^{\infty} d\vec{H} = \int_{z=-\infty}^{\infty} \frac{I r dz \vec{a}_\phi}{4\pi (r^2 + z^2)^{3/2}}$$

By substitution method,

$$z = r \tan \theta \quad dz = r \sec^2 \theta d\theta$$

$$\therefore \vec{H} = \int_{\theta=-\pi/2}^{\pi/2} \frac{I r r \sec^2 \theta d\theta \vec{a}_\phi}{4\pi (r^2 + r^2 \tan^2 \theta)^{3/2}}$$

$$\boxed{\vec{H} = \frac{I}{2\pi r} \vec{a}_\phi} \quad \text{A/m} \quad (1)$$

$$B = \mu H$$

$$\boxed{\vec{B} = \frac{\mu I}{2\pi r} \vec{a}_\phi} \quad \text{wb/m}^2 \quad (1)$$

B2) a) iii)

Given:

- $N = 500$ turns
- $A = 2 \text{ cm}^2 = 2 \times 10^{-4} \text{ m}^2$
- $R = 10 \text{ cm} = 10 \times 10^{-2} \text{ m}$
- $\mu_r = 800$

To find:

Self Inductance

Solution:

$$L = \frac{\mu N^2 A}{2\pi R} \quad (2)$$

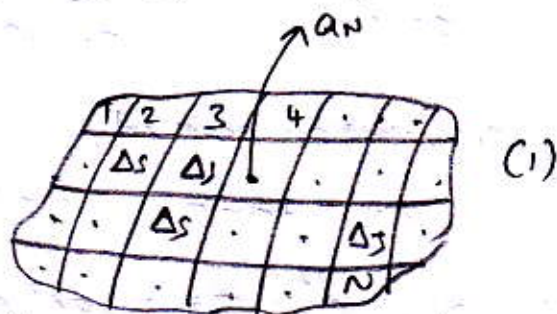
$$\mu = \mu_0 \mu_r = 4\pi \times 10^{-7} \times 800$$

$$L = \frac{4\pi \times 10^{-7} \times 800 \times (500)^2 \times 2 \times 10^{-4}}{2\pi \times 10 \times 10^{-2}} = 0.12 \text{ H}$$

$$\boxed{L = 120 \text{ mH}}$$

B2) b) i) Stokes Theorem:

The Stokes theorem states that "the line integral of vector \vec{A} around a closed path L is equal to the integral of curl of \vec{A} over the open surface S enclosed by the closed path L ".



$$\oint \vec{H} \cdot d\vec{l} = \int_1 \vec{H} \cdot d\vec{l} + \int_2 \vec{H} \cdot d\vec{l} + \dots + \int_N \vec{H} \cdot d\vec{l} \quad (1)$$

from curl definition,

$$\lim_{\Delta S \rightarrow 0} \frac{\oint \vec{H} \cdot d\vec{l}}{\Delta S} = (\nabla \times \vec{H})_n \quad \text{--- (1)} \quad (1)$$

$$\oint \vec{H} \cdot d\vec{l} = \lim_{\Delta S \rightarrow 0} (\nabla \times \vec{H})_n \Delta S \quad \text{--- (2)} \quad (1)$$

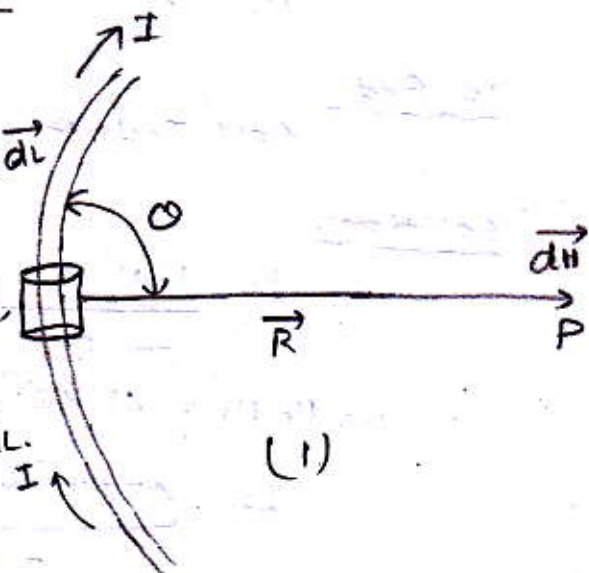
$$\oint \vec{H} \cdot d\vec{l} = (\nabla \times \vec{H}) \cdot \vec{n} \Delta S$$

$$\boxed{\oint \vec{H} \cdot d\vec{l} = (\nabla \times \vec{H}) \cdot \vec{n} \Delta S} \quad (2)$$

B2) b) ii) Biot - Savarts law:

Biot Savarts law states that, The magnetic field intensity \vec{H} produced at a point P due to a differential current element $I d\vec{l}$ is,

1. proportional to the product of current I and differential length $d\vec{l}$.



(1)

2. The sine of the angle b/w the element and $\textcircled{7}$ the line joining point P to the element

3. And inversely proportional to the square of the distance R b/w point P and the element. $\textcircled{1}$

Mathematically, the Biot-Savart's law can be stated as,

$$d\vec{H} \propto \frac{I dL \sin\theta}{R^2} \quad \text{--- } \textcircled{1}$$

$$d\vec{H} = \frac{K I dL \sin\theta}{R^2} \quad \text{--- } \textcircled{2} \quad K \rightarrow \text{constant of Proportionality}$$

$$d\vec{H} = \frac{I dL \sin\theta}{4\pi R^2} \quad \text{--- } \textcircled{3} \quad K = \frac{1}{4\pi} \quad (1)$$

from rule of cross product

$$d\vec{L} \times \vec{a}_R = dL |\vec{a}_R| \sin\theta = dL \sin\theta \quad \text{--- } \textcircled{4} \quad (1)$$

using $\textcircled{4}$ in $\textcircled{3}$ we get

$$d\vec{H} = \frac{I d\vec{L} \times \vec{a}_R}{4\pi R^2} \quad \text{A/m}$$

$$\vec{a}_R = \frac{\vec{R}}{|\vec{R}|} = \frac{\vec{R}}{R}$$

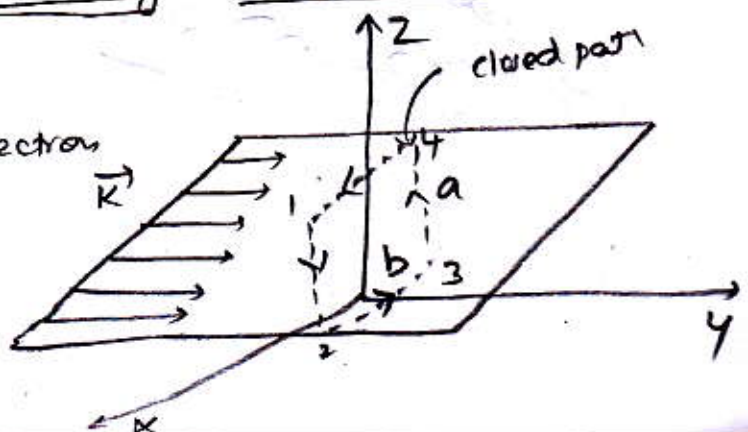
$$\boxed{d\vec{H} = \frac{I d\vec{L} \times \vec{R}}{4\pi R^3}} \quad \text{A/m} \quad (1)$$

The above eq. is the mathematical form of Biot Savart's law.

B2) b) iii) Magnetic field intensity - Infinite sheet:

Current flowing in y direction

$$K = K_y \hat{a}_y$$



Applying Ampere's circuital law

$$\oint \vec{H} \cdot d\vec{l} = I_{\text{enclosed}}$$

$$\oint \vec{H} \cdot d\vec{l} = \int_1^2 + \int_2^3 + \int_3^4 + \int_4^1 (\vec{H} \cdot d\vec{l}) \quad (1)$$

From closed path, 1-2 and 3-4 the integrals

$$\int_1^2 \vec{H} \cdot d\vec{l} + \int_3^4 \vec{H} \cdot d\vec{l} = 0$$

consider path 2-3,

$$\int_2^3 \vec{H} \cdot d\vec{l} = \int_2^3 (-H_x \vec{a}_x) \cdot (dx \vec{a}_x) = b H_x \quad (1)$$

consider path 4-1

$$\int_4^1 \vec{H} \cdot d\vec{l} = \int_4^1 (H_x \vec{a}_x) \cdot (dx \vec{a}_x) = b H_x \quad (1)$$

$$\oint \vec{H} \cdot d\vec{l} = b H_x + b H_x = 2b H_x = I_{\text{enclosed}}$$

$$2b H_x = K_y b$$

$$\boxed{H_x = \frac{1}{2} K_y} \quad (1)$$

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